ANTENNAS FABRICATION FOR RFID UHF AND MICROWAVE PASSIVE TAGS

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ABSTRACT: In this paper, the authors present several antenna structures for RFID passive tags with direct chip connection. In this study, the substrate is PET (Polyethylene terephthalate) with 80µm thickness, the conductive layer is copper with 10µm thickness and CST Microwave Studio is used for simulation. The antenna design process is described and related results are shown. The goal of this study is to achieve compact size, good matching impedance, and to increase the bandwidth and read range of the tag as much as possible. The prototypes were fabricated by sputtering technology with 1µm thickness, then thickened by electroplating technique and finally tested by hand-held reader for read range characterizations.

Keywords: RFID; UHF RFID tag; dual-band antenna; XRAG2 chip; Atmel ATA5590 chip; radiation pattern; PET substrate.

1. INTRODUCTION

RFID technology is a technology perfectly suited for our ubiquitous world. To get and retrieve information on an object, tags are very useful. And they are particularly useful in the case of logistics. At the moment, there is still a large use of barcodes, but the line-of-sight reading causes various inconvenient in real environment. Nowadays, RFID is more and more interesting and already used for some applications. This paper focuses on the antenna designs for RFID passive tag in UHF band and at 2.45 Ghz. In fact, at the Laboratory for Nanotechnology (LNT), a platform for RFID research was established in order to perform studies on passive RFID tags and to realize some RFID system prototype based on the antenna design and RFID tags fabricated in our facility.

Our designs are divided into two directions: (i) first to match with XRAG2 passive chip (for first design in the UHF band) and (ii) with Atmel ATA5590 chip (for second design at 2.45 Ghz and third design in dual-band). Our target is to operate in the UHF band and at 2.45 Ghz, to have an omni-directional radiation pattern with sufficient gain, to extend the bandwidth and to increase the read range.

This paper is further organized as follows: Section II presents the antenna designs procedure using CST Microwave Studio for the antenna structures mounted with XRAG2 chip and Atmel ATA5590 chip. The fabrication process, the tag prototype, the result of the measurement and the read range are shown in
this section. And finally, the conclusions are given in Section III.

2. ANTENNA DESIGN PROCEDURE

The first attempt has been made for applications in UHF band using XRAG2 chip having the input impedance of 23-180j Ohm at 915 Mhz. With this antenna, the first task was to make the resonant frequency be in UHF band, therefore the study about the resonant frequency of the antenna on the PET substrate have to be done. Through the simulation, it was found that the resonant frequency of the antenna would be shifted after mounting the chip. So a loop of about 75mm at 868MHz was chosen as the first component of the antenna structure. After having the desired resonant frequency, next is to focus on the impedance matching and on expanding the bandwidth of the antenna. With double loop, the impedance matching would be better but dimensions of the loop have to be adjusted for obtaining the desired resonant frequency. To expand the bandwidth, the second resonant frequency was created by adding the tip-load [1], [2]. And then, the second resonant frequency was moved close to the first one by adjusting the tip-load’s size. After analyzing the influence of the dimensions of antenna, it is noted that increasing the length and reducing the width of the loop can compact the size but still achieve the desired resonant frequency while the return loss is better. Besides, using four symmetrical tip loads is easier to pull the resonant frequencies as well as to have better matching impedance.

![Figure 1.](image1.png)

**Figure 1.** a) The first antenna and its, b) Return loss, c) Impedance smith chart, d) Radiation pattern.
In the following step, the parameters of some components were varied to optimize the resonant frequency and the matching impedance with the chip. The first antenna structure with its radiation characteristics are shown in Fig. 1.

The bandwidth of -10 dB is around 100 MHz, covers the UHF band for RFID. The impedance matching is not good but can be accepted. And the radiation pattern is good with the gain of 1.9 dBi.

![Antenna Structure](image)

**Figure 2.** a) The second antenna and its, b) Return loss, c) Smith chart, d) Radiation pattern.

Our second design was matched with the Atmel ATA5590 chip having the input impedance of $10.5 - 143j$ Ohm at 915 MHz and $10 - 31j$ Ohm at 2.45 GHz. This design was just focused at 2.45 GHz, so the compact size problem was already done since the higher working frequency gives the smaller antennas structure. With this frequency, the design began from straight dipole configuration [1-4] with the length of about 32 mm. The length and width of dipole was adjusted to obtain the desired resonant frequency. And then, the other components as the jamb, the stub were added to match impedance with chip. These components did not affect too much to radiation pattern of antenna. Besides, they can extend the bandwidth of antenna.
At last, through simulations, the parameters of antenna were adjusted again to optimize the characteristics. The second design and its characteristics are shown in Fig. 2. The bandwidth of -10 dB is around 106 Mhz, ensures the tag can work properly at 2.45 Ghz. The impedance matching has a good result for simulation and the radiation pattern is good too with the gain of 1.9 dBi.

Our next antenna was also designed with Atmel ATA5590 chip, but it was supposed to have dual-band antenna feature [5]. It has two resonant frequencies: one in UHF band and another at 2.45 GHz. This design had the same initial idea with the second design, use a straight dipole for the first resonant frequency. And then, a circle component was added, it links two parts of dipole together. This made the second resonant frequency to be appeared. But these resonant frequencies were not in correct positions. Therefore, the jamb and the stub were added to obtain the desired resonant frequencies and to match impedance with chip. And finally, the parameters of the antenna were adjusted to obtain the best result.

It is noted that this is a dual-band antenna, so this antenna was matched with impedance of the chip in UHF band and at 2.45 GHz.

Figure 3. a) The third antenna, b) Effect of “a” at 2.45 Ghz, c) Effect of “a” in UHF band, d) Effect of “d” at 2.45 Ghz, e) Effect of “d” in UHF band, f) Effect of “f” at 2.45 Ghz, g) Effect of “f” in UHF band, h) Effect of “i” at 2.45 Ghz, i) Effect of “i” in UHF band
independently. The components that are close
the chip (except the circle) effects to
characteristics of antenna at 2.45 GHz so much,
but almost does not effect in UHF band. And
the other components effect to characteristics
of antenna in both bands. The third design and
some effects of the antenna’s parameters are
shown in Fig. 3 (all dimensions are in mm).

From Fig.3b and 3c, it is found that the
return loss at 2.45 Gbh is affected strongly by
“a”. But in UHF band, the effect of “a” is very
small. In Fig. 3d and 3e, the return loss at 2.45
Gbh is also affected by “d”, but the effect is not
as strong as in case “a”. Because of “a” is
closer to chip than “d”. And in UHF band, the
effect of “d” is almost nothing. From Fig. 3f,
3g, 3h and 3i, it is obviously that the effects of
“i” and “f” on the return loss at 2.45 Gbh are
weaker. But in UHF band, it is found that the
effects are stronger. With this design, “a” has
a strongest effect on the return loss at 2.45
Gbh. Therefore, it can be used to adjust for
impedance matching at 2.45 Gbh first. And
then, the others will be used to match
impedance in UHF band. And its
characteristics are shown in Fig. 4. The
bandwidth of -10 dB is around 26 Mhz in UHF
band and the return loss at near 2.45 Gbh is
10.7 dB, but it can be still accepted. The
impedance matching is not good but it ensures
that it is for both bands. The radiation pattern at
2.45 Gbh is rather distorted, but with the high
gain of 3.6 dBi, it can be compensate for the
bad return loss. And the radiation pattern in
UHF band is good with the gain of 1.9 dBi.

The testing the first antenna with 500mW
hand-held reader was performed, the maximum
read range about 60 cm was obtained.

The prototypes have been made at
Laboratory for Nanotechnology (LNT),
Vietnam National University - Ho Chi Minh
City by sputtering technology. And then, they
have been tested by using Rohde & Schwarz
ZVB Vector Network Analyzer available at
Department of Telecommunication
Engineering, HCMC University of
Technology. The real antennas are shown in Fig. 5a, 5b, 5c. And the experimental
results of the antennas are shown in Fig. 6. The
obtained results in UHF band are rather similar
to the simulated results, but they are not really
good at 2.45 Gbh. In the measurement process,
the measured conditions which are not good
enough for measuring at 2.45 Gbh can make
this distortion.
Figure 4. a) Return loss at 2.45 GHz; b) Return loss in UHF band; c) Impedance smith chart; d) Radiation pattern at 2.45 GHz; e) Radiation pattern in UHF band.
3. CONCLUSIONS

In this paper, the antenna design processes with direct chip connection have been presented. With all designs, we try to obtain the best impedance matching in UHF band (860-960 MHz) and at 2.45 GHz. Three antenna structures have been designed and fabricated with size can be fixed in an identification card. The first design has large bandwidth cover all frequency in UHF band, this advantage make this antenna can be applied in many countries. The second and third designs are prospective designs for applications at 2.45 Ghz and in dual-band. These tags can be fabricated easily and some of them can be tested by hand-held reader with the maximum read range can be as far as 60 cm. These tags are entirely possible to be realized in practice. In future, we hope to optimize these designs to obtain better characteristics.
CHẾ TẠO ĂNG-TEN CHO THẺ RFID THỤ ĐỘNG Ở BĂNG TẦN UHF VÀ VI BA

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Tóm tắt: Trong bài báo này, chúng tôi đưa ra một vài cấu trúc ăng-ten cho thẻ RFID thụ động với quy trình kết nối chíp trực tiếp. Trong nghiên cứu này, lớp điện được sử dụng là PET (Polyethylene terephthalate) với độ dày là 80µm; dải dẫn làm bằng đồng với độ dày là 10µm; và phần mềm được sử dụng để mô phỏng là CST Microwave Studio. Quá trình thiết kế ăng-ten được trình bày kỹ cẩn và các kết quả liên quan cũng được đưa ra. Mục tiêu của nghiên cứu này là cố gắng tạo ra thẻ nhận dạng có kích thước bé, phối hợp tốt không tốt, và quan trọng là bandwidth và tầm đọc của thẻ càng tăng nhiều càng tốt. Các mẫu chế tạo được thực hiện bằng phương pháp phun xạ với độ dày 1µm.

\(\text{Figure 6. Measured input impedance of: a) the first antenna with various thicknesses; b) the second antenna with various thicknesses; c) the third antenna with various thicknesses.}\)
sau đó được tiếp tục làm dày bằng phương pháp điện hoá và cuối cùng được kiểm tra tầm đọc bằng đầu đọc cầm tay.

Từ khoá: RFID; thẻ UHF RFID; ăng-ten hai băng tần; chíp XRAG2; chíp Atmel AT5590; đồ thị bức xạ; đế PET.

REFERENCES